

On-line Inspection of the Surface Roughness of Workpiece in Ultraprecision Machining

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Abstract: An in situ technique to determine the surface roughness of ultraprecision machining using optical characteristic effects is fundamental as probes are not used, which prevents contact damage on the surface. Because the plastic lens molding reprints the roughness of the mold core fabricated by machining, tool marks result in the poor surface of the plastic lens. The machined surface can reflect the input light of a green laser with a short wavelength of 532 nm. By varying the feed rate of the ultraprecision machining, several samples of the electrolyte-less nickel with different surface roughness have been examined using the green laser and the photodiode array. The distribution of the optical scattering effect of each sample under the light source of green laser is derived for prediction of the surface roughness. The results show that greater surface roughness produces more expansive distribution of light scattering. In addition, the bidirectional scatter distribution function (BSDF) of the machined surface is found to be proportional to roughness. Using the ratio of the main and the side measuring channels of the photodiode array, a suitable approach to establish the relationship between light scattering and surface roughness can be developed. The laser and the photodiode array are found to efficiently predict the surface roughness of the ultraprecision machined electroless nickel.

Introduction

Surface roughness is typically used to describe the level of the machining mark on the workpiece. Generally, a stylus measures the surface roughness of the machined workpiece in industrial applications. However, this contact method may damage the workpiece surface and does not help in the complete inspection of the workpieces. Hence, a noncontact method for measuring the surface roughness is vital. Among the noncontact methods, optics-based approaches, including by light scattering and digital image approaches, are the primary noncontact methods for surface roughness measurement.

The injection molding process reprints the surface roughness of machining from the mold core to the plastic lens. The reprinted surface roughness of the plastic lens produces light scattering effect, while the light is transmitted to and/or reflected from the interface of the plastic and air. Thus, the induced light scattering produces stray light in the optical system, which affects the performance of the lens system. Theoretical investigation of light scattering induced by surface roughness is complicated, due to the fluctuation in the profile with numerous irregularities. Zhao and Gao (2009) indicated that the speckle contrast method and the light scattering method are two of the most noncontact techniques for on-line surface roughness measurement of slightly-rough surface. The influence from the diffuse component of scattered light may eliminate.

Many studies have been carried out to investigate light scattering induced by surface roughness, including those by Tanner and Fahoum (1976), who measured the reflected light intensity from the mirror surface to derive the relationship between roughness and scattering effect by the angular resolved method. The measured reflected light intensity from the mirror surface to derive the relationship between roughness and scattering effect. Beckmann (1987) constructed model of the ratio of the scattering intensity to the reflected light intensity by launching the laser on the surface while considering the roughness magnitude and the related characteristic surface parameters. Based on the Beckmann model, Persson (1998) used an in-process measuring scheme to predict the surface roughness in grinding with a laser. Vandembroucq et al. (2001) revealed that previous research incorrectly measured the surface roughness and the induced light scattering by neglecting the effects of multi-scattering and shadowing. The light scattering technique can be used to predict the surface roughness of steel in the turning process (Wang et al., 2000) and of a silicon wafer in the grinding process (Tay et al., 2004).

To derive the relationship between surface roughness and scattering effect, Fontani et al. [2000] measured the light scattering of the machining parts with flat surface by eight photodiode sensors and He-Ne laser of 632.8 nm wavelength. These sensors recorded 90° radial distribution of scattering light. Furthermore, Fontani et al. [2001] used a linear array of sensing detector with 16 photodiodes to derive the ratio of scattering to reflective light intensity induced by the machining mark on the crankshaft. The surface roughness of the crankshaft was predicted using this ratio. However, the positioning of the light source and the sensing detector was more complicated.

The mold core surface, subjected to ultraprecision machining, is usually assumed to be mirror-like for the design of plastic light-guide components. However, the tool marks during machining can cause poor surface of the plastic lens. Beckmann [5] proposed the following model for the description of electromagnetic scattering induced by random scratching surface:

$$\frac{I_s}{I_o} \propto \left[- \left(\frac{4\pi R_q \cos \theta}{\lambda} \right)^2 \right] \quad \text{for } \frac{I_s}{I_o} > 0.6 \quad (1)$$

where I_s is the mirror specular light intensity, I_o is the whole reflective light intensity, θ is the incident angle, and R_q is the root mean square of surface roughness.

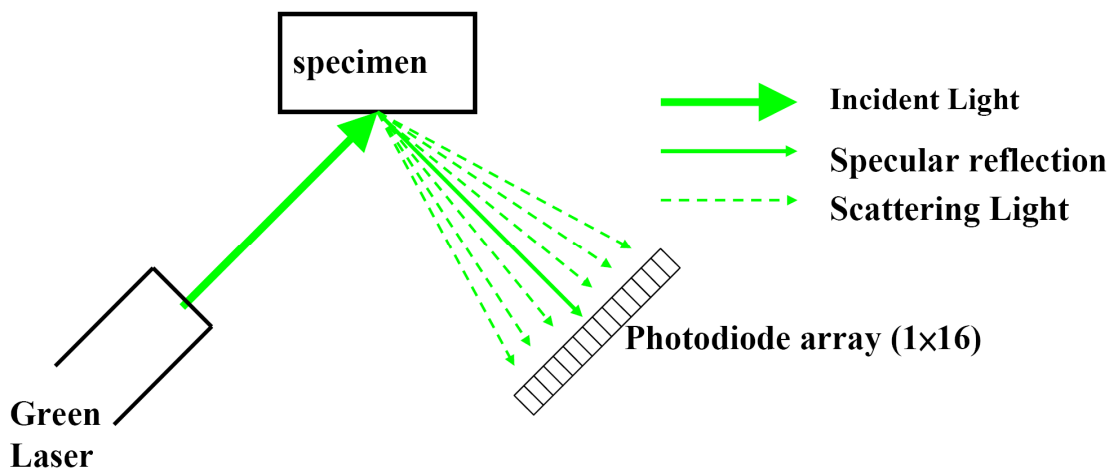


Fig. 1 Incident angle, light scattering angle and the reflective specular light

The specular light intensity from the surface is decreased, while the scattering light intensity is increased, with respect to the increased roughness. Using the ratio of scattering light intensity near

the imposed point to the one far from the imposed point, Cahill [2001] tried to derive the roughness of the machining surface. As analysis of the light scattering effect induced by surface roughness is sophisticated, Church et al. [1977] first predicted the roughness by the bidirectional scatter distribution function (*BSDF*). However, Stover [1995] showed that light scattering of the interface of media can be defined by either *BSDF* or total integrated scattering (*TIS*). The *BSDF* can be obtained using the following expression: *BSDF* = differential radiance/differential irradiance. In Fig. 1, the *irradiance* indicates the ratio of the laser power imposed on the spot of the surface to the area of the spot (P_{laser}/A_{spot}), and thus, the radiance can be given as

$$radiance = P_{scatter} / (\Omega_s \cos \theta_s A_{detector}) \quad (2)$$

where Ω_s is the solid angle, $P_{scatter}$ is the scattering light intensity of the photosensor received, θ_s is the scattering angle, and $A_{detector}$ is the receiving area of the photosensor. Hence,

$$\begin{aligned} BSDF &= (P_{scatter} / \Omega_s \cos \theta A_{detector}) / (P_{laser} / A_{spot}) \\ &= P_{scatter} A_{spot} / \Omega_s \cos \theta A_{detector} P_{laser} \end{aligned} \quad (3)$$

Once $A_{detector} = A_{spot}$, Eq. (3) can be simplified as $BSDF = (P_{scatter} / P_i \Omega_s \cos \theta_s)$. In fact, for a metal workpiece, the main scattering occurs from the reflectance.

The *BSDF* can be simplified as *BRDF* (Bidirectional Reflectance Distribution Function), by neglecting the transmission into the interface. For ultraprecision machining process, the surface roughness of the workpiece is important during the application of plastic lens molding. As contact probing is used to determine the surface roughness, which may damage the mirror-like surface, a contactless measurement technique can thus be useful for the ultraprecision process. However, in the interferometer approach, the measurement cost is more expensive owing to the higher equipment cost. As scattering effect can help determine surface roughness, Beckmann [1987], Persson [1998], and Vandembroucq et al. [2001] tried to predict the surface roughness using laser scattering.

Elson and Bennett [1989] showed that if the irregularity size of the surface profile is similar to or smaller than that of the reflected light, then light scattering should be analyzed by refraction theory. They found that the angular distribution of scattered light from optical surfaces as a function of the wavelength. However, there is no literature on the surface roughness measurement for ultraprecision machining using light scattering effect of green laser. Shorter wavelength than the He-Ne laser, the green laser may give an accurate solution in this study. Hence, the purpose of this study was to investigate the surface roughness of ultraprecision workpiece using light scattering effect. Several samples of electroless nickel with different surface roughness obtained by varying the feed rate of the ultraprecision machining were examined by the green laser. The 1×16 photodiode array with a 2-mm pitch was constructed to measure the distribution of the optical scattering effect under the light source of the green laser.

Experimental Setup

In this study, electroless nickel workpieces were machined using an ultraprecision lathe to derive different levels of surface roughness. Fixing the the revolution frequency of the workpiece at 2400 rpm and the cutting depth of the diamond tool at 1μm, the different levels of surface roughness derived from varying the feedrate of the diamond tool. On pointing the coherent laser on the surface of the workpieces, the photodiode array was able to detect the light scattering effects of the samples with different surface roughnesses. The wavelength and power of coherent green laser are 532 nm and 5 mW, respectively. Besides, the S5668 Hamamatsu silicon photodiode array of had a 1×16 linear of pitch of 1.6 mm. With the coherent laser's incident angle on the surface of the

workpieces, the reflected specular light from the surface was set on the 8th channel of the photodiode array to describe the scattering distribution. An Advantech PCI-1710 AD/DA acquisition card was used to transfer the sensing voltage of each element of the photodiode array to the desktop computer.

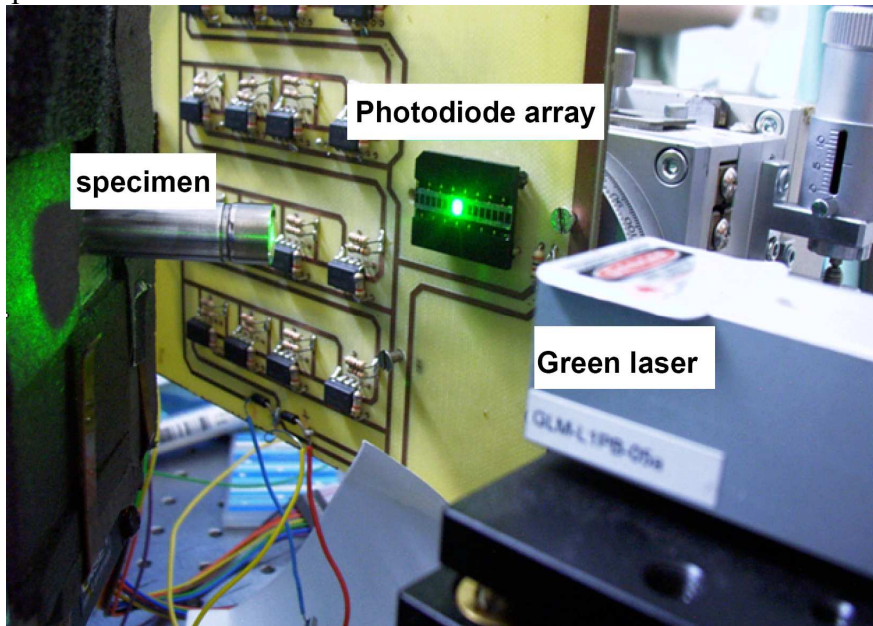


Fig. 2 The experimental setup includes the green laser, a workpiece, a photodiode array and amplified circuits

Figure 2 shows the experimental setup where the green laser has an incident angle of 45° to the machined end surface of the electroless nickel workpiece. According to the Fresnel theorem, the incident angle equals the reflective angle where the normal line is perpendicular to the machined end surface of the workpiece. The reflected light with scattering effect was collected by the photodiode array. The distance between the workpiece and the photodiode was either 26 or 50 mm. Figure 3 shows the scattering effect induced by surface roughness (R_q) of 48.7 nm by green laser. The light has been spread expansively associated with the diffractive effect by the surface roughness of the workpiece in ultraprecision machining, which is in agreement with the previous literature findings.

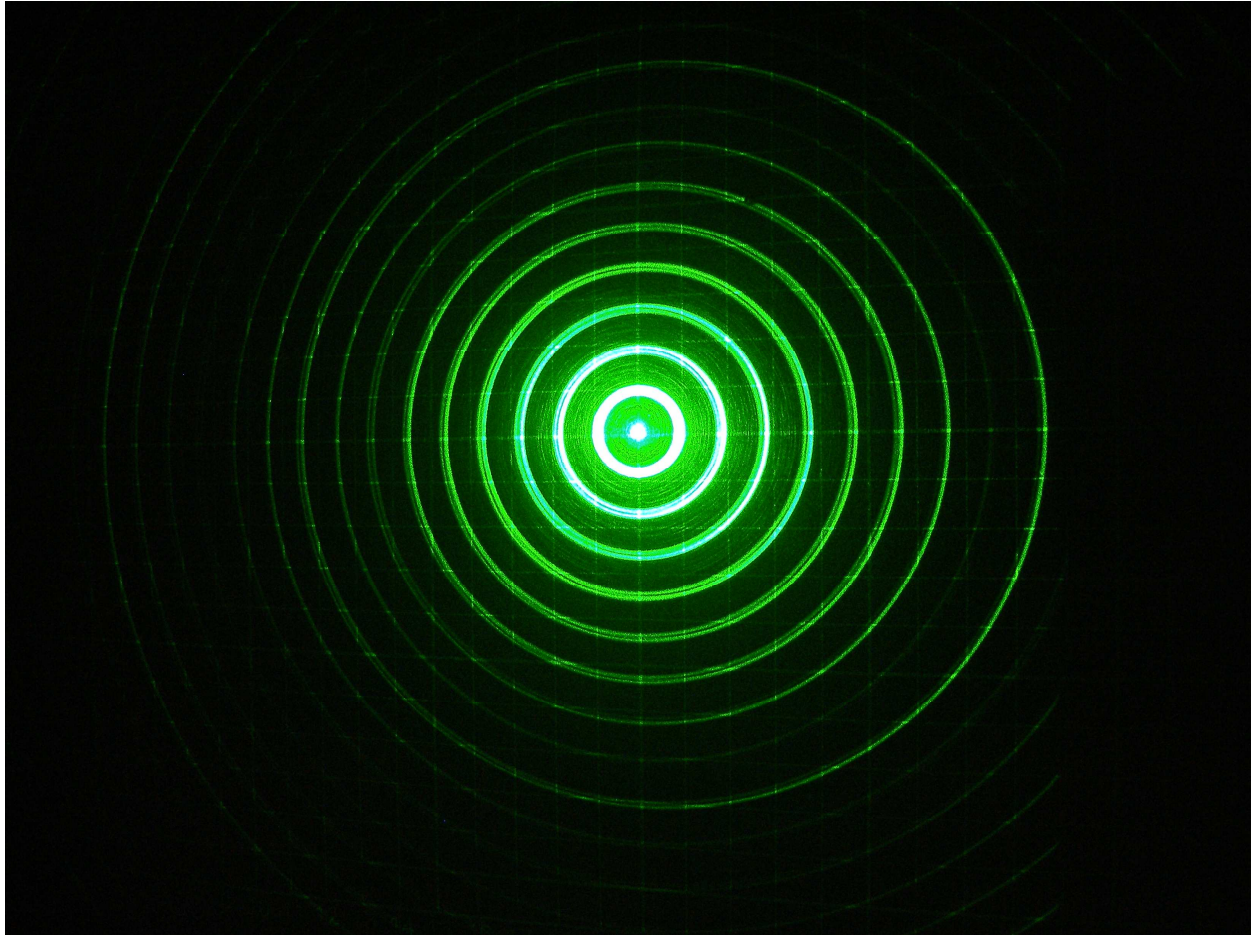


Fig. 3 The scattering effect induced by surface roughnesses (R_q) of 48.7 nm by green laser

Results and Discussion

In the previous experimental setup of laser incident angle of 45° and different levels of the surface roughness workpiece, the photodiode array measured the scattering distribution from the end surface of the workpiece at distances of 26 and 50 mm. Figure 4 shows that the received intensity (voltage) of the specular channel increased with the lower surface roughness. The regressive equation fits well to the row experimental data thanks to the higher R^2 . By the equation, the received intensity from the rough surface under ten percent of the wavelength of incident green laser is 3.679 (V) while the perfect surface without the roughness gives the received intensity is 4.215 (V). The analysis reveals that the surface roughness below one tenth of the incident light wavelength induces about 13 % loss of the specular light. Due to the plastic injection molding is an imprint process, the surface roughness of the mould is printed on the molding parts. The surface roughness requirement of the plastic optical lens should be more restrict for the higher specular light intensity and the lower light scattering.

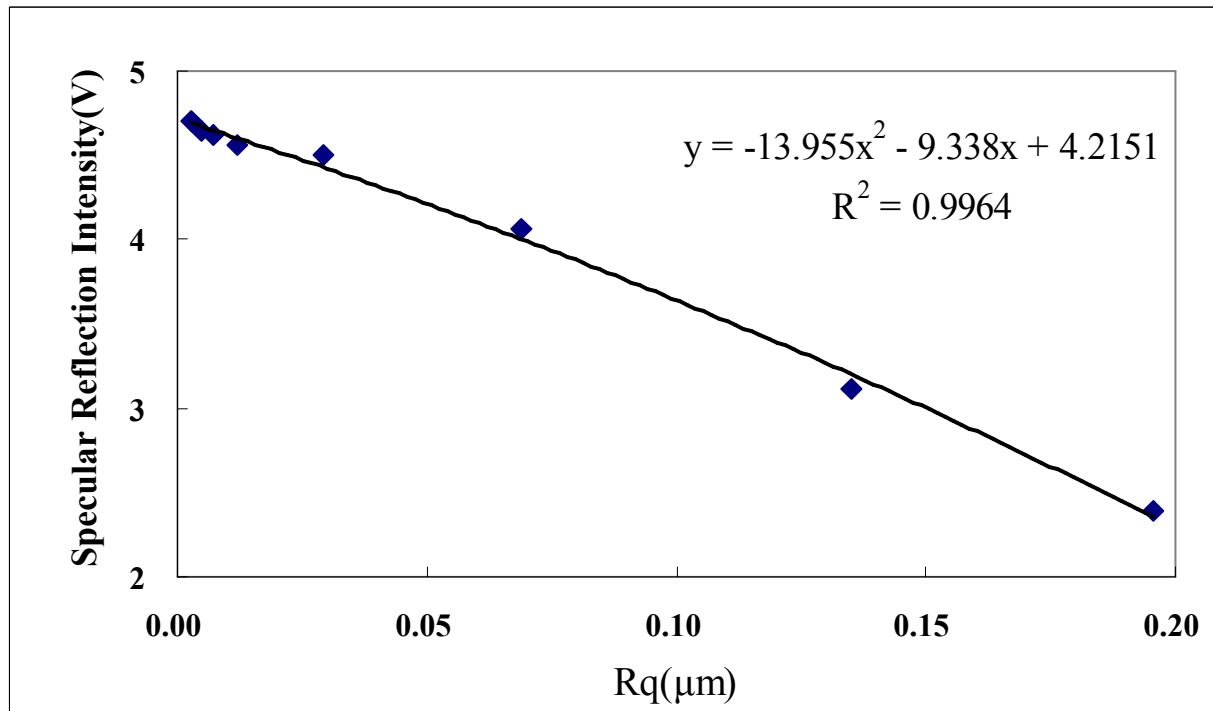


Fig. 4 The specular reflection intensity from the machined electroless nickel at an incident Angle of 45-° and 26-mm Distance by green laser of 532nm.

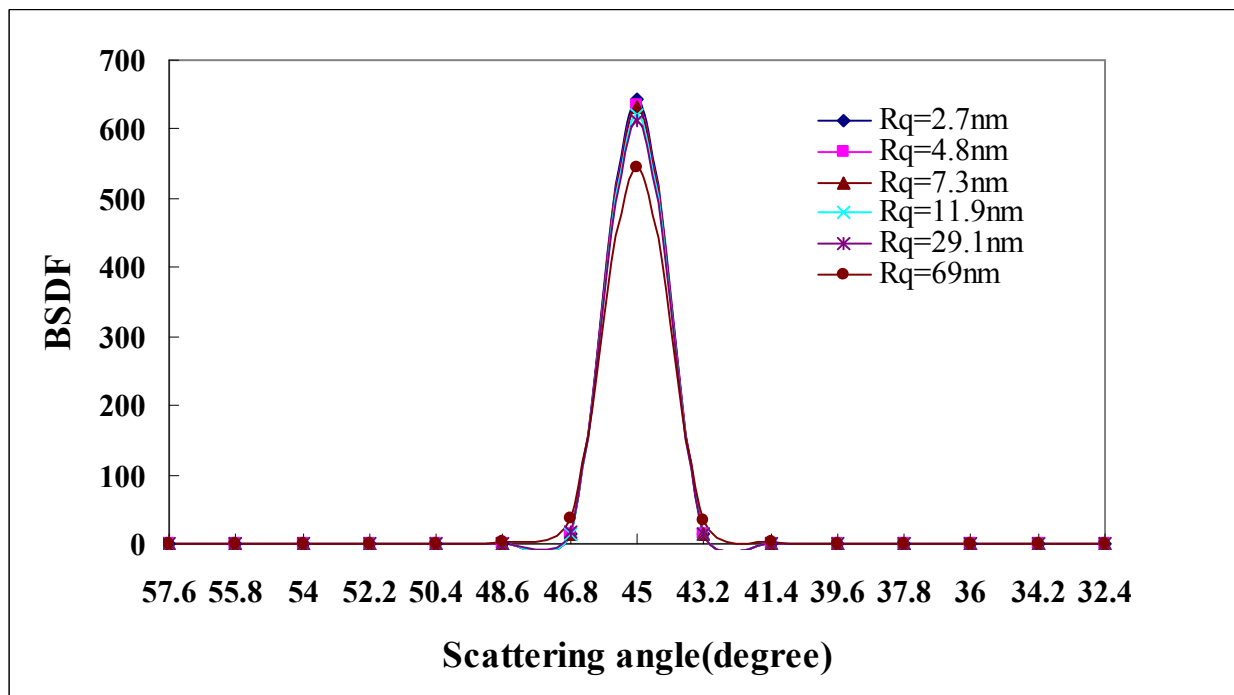


Fig. 5 (a) Light Scattering Reflectance from the Machined Electroless nickel at an Incident Angle of 45-° and 26-mm Distance

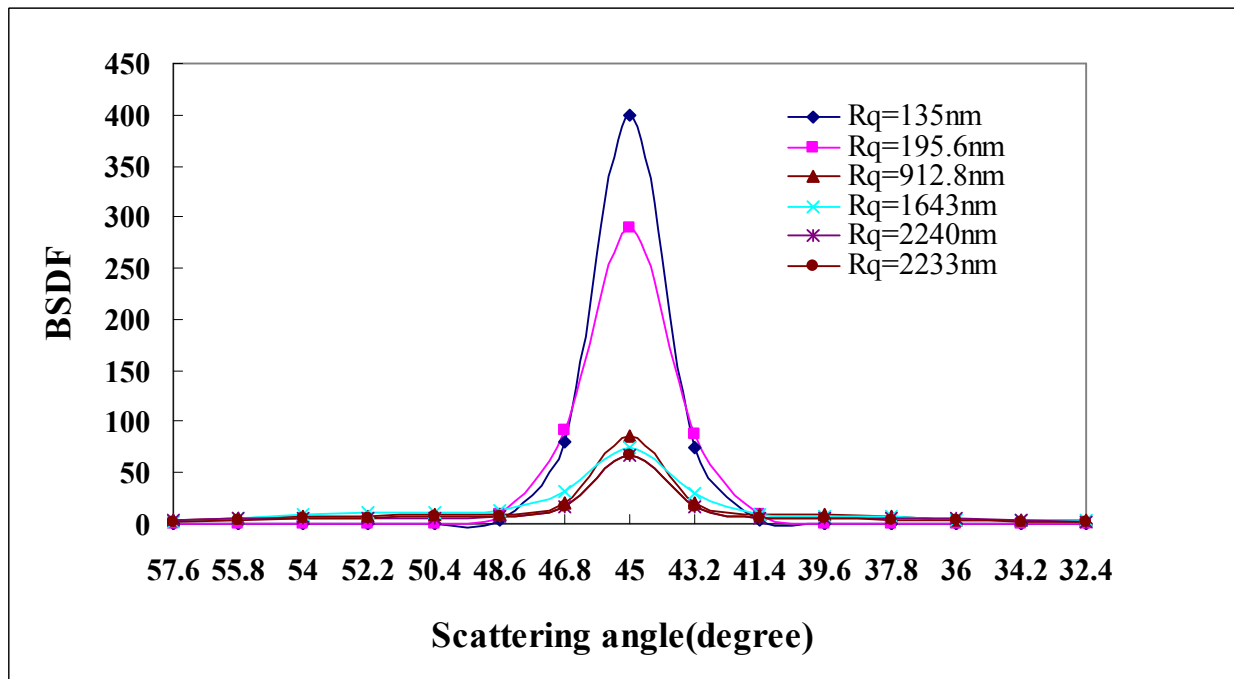


Fig. 5 (b) Light Scattering Reflectance from the Machined Electroless nickel at an Incident Angle of 45° and 26-mm Distance

Conclusions

The received intensity of the specular channel was found to increase with decrease in the surface roughness, which is in agreement with earlier studies. In addition, the scattering light was found to be of Gaussian distribution once the surface roughness became smaller. This phenomenon of the light scattering distribution became wider when the surface roughness was becoming worse. However, a larger distance was found to enhance the BSDF values owing to a larger receiving angle of each element of the photodiode array, i.e., for each element of the photodiode, the receiving angle increased with respect to the increased distance. The BSDF of the machined surface was found to be proportional to the roughness. Using the ratio of the main and side measuring channels of the photodiode array, a suitable approach to determine the relationship between light scattering and surface roughness has been developed. Thus, the laser and the photodiode array effectively predicted the roughness of the ultraprecision machined surfaces of the electroless nickel. This study developed a feasible online measurement technique to determine the roughness of ultraprecision machined surface by reflected light scattering effect.

Acknowledgments

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