

## 1.2 kV SiC MOSFET with Low Specific ON-Resistance and High Immunity to Parasitic Turn-On

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**Abstract.** With the capability to switch at high speed, there are important concerns about Parasitic Turn-On (PTO) when using SiC MOSFETs in switching applications with fundamental half-bridge configuration [1]. In this work, we present 1200V SiC planar MOSFETs with low specific ON-resistance ( $R_{sp}$ ), fast switching characteristics and high immunity to PTO. The PTO immunity is verified by experimental comparison to several commercially available SiC MOSFETs.

### Introduction

SiC MOSFETs are now widely used in numerous applications, especially automotive applications such as traction inverters and fast charging stations. Thanks to its superior physical properties, SiC MOSFETs are expected to operate with low  $R_{DS(on)}$  and fast switching condition. Nevertheless, under fast switching condition in half-bridge configuration, complementary device, i.e., Body Diode (BD) can experience unwanted PTO [1, 2].

PTO is described as an unwanted effect during MOSFET switch turn-on, i.e., BD turn-off. Here, while BD  $V_{DS}$  rising to take  $V_{DD}$ , device's internal nonlinear capacitances like  $C_{GS}$ ,  $C_{GD}$  and  $C_{DS}$  are also in transient mode. Charging current from  $C_{GD}$  unwantedly charge  $C_{GS}$  as well as gate resistor  $R_{G\_EXT} + R_{G\_INT}$  and pull-up the HS  $V_{GS}$ . If the HS  $V_{GS}$  is pulled over device's  $V_{TH}$ , the BD channel will open under a high  $V_{DS}$  voltage. The HS  $V_{GS}$  pulled-up event during BD turn-off was described as [2]:

$$\frac{dV_{GS}}{dt} = \frac{1}{C_{GS}} \left[ C_{GD} \frac{dV_{DS}}{dt} - \frac{V_{GS}}{R_G} \right] \quad (1)$$

Equation (1) qualitatively stated that, HS  $V_{GS}$  pull-up depend on device's  $C_{GS}$ ,  $C_{GD}$ , switching speed and total  $R_G$ . There were efforts on design novel gate drivers to limit PTO when using SiC MOSFETs in switching application [3]. Therefore, from device design perspective, it is important to design and optimize the device structure to obtain SiC MOSFETs that are highly robust against PTO.

In this work, we introduce 1200V SiC MOSFETs with low  $R_{DS(on)}$ , fast switching characteristics and an optimized capacitance  $C_{ISS}/C_{RSS}$  ratio for a highly robust device against PTO.

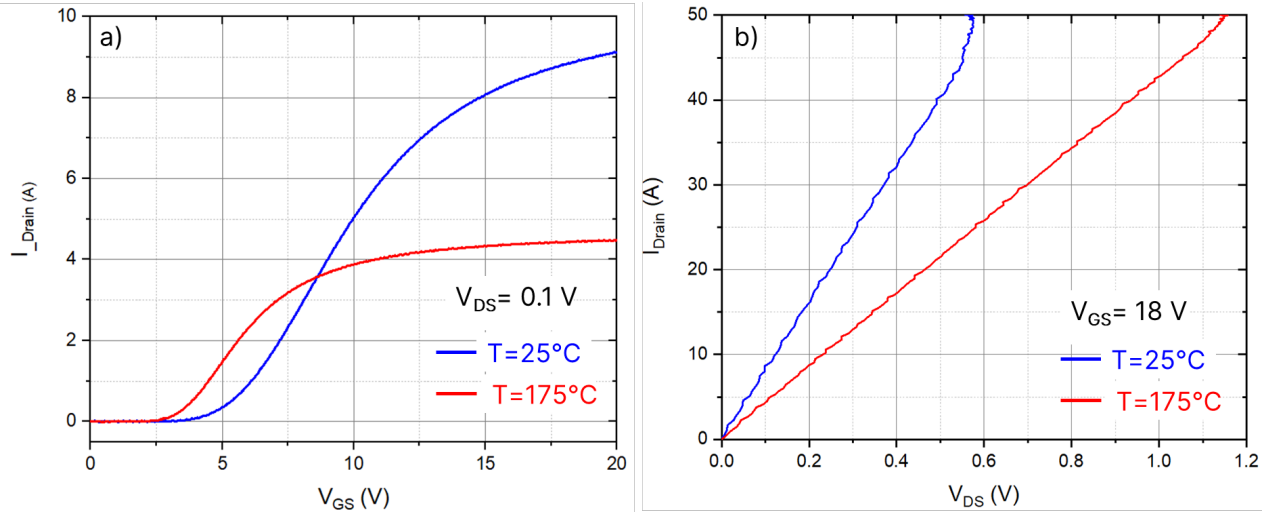
### Device Fabrication and Measurements Set-up

Planar implanted SiC MOSFETs with a total chip area of  $24.6\text{mm}^2$  and optimized cell design for 1200V were fabricated using 150mm SiC epitaxial wafers. Devices were then packaged and measured in TO-247-4L housing. A Keithley S500 integrated test system were used for DC measurements and pulsed high current measurements, using a pulse width of 230  $\mu\text{s}$ . Double Pulse Tester (DPT) were used for switching measurements and PTO evaluation. In our switching measurements, the Low Side (LS) device is the active switch and High Side (HS) device is the BD.

Simplified device structure, measurements set-up and simplified circuit diagram were described elsewhere [4,5].

### DC Characteristics

Fig.1a represents the typical measured device's transfer characteristics at RT and at 175°C, with  $V_{DS}=0.1V$ . Device's typical  $V_{TH}$  is 3V at RT and 2V at 175°C, respectively (with  $V_D=V_G$  @ $I_D=33mA$ ). Fig.1b shows measured output characteristics at RT and 175°C, with  $V_{GS}=18V$ . Device's typical  $R_{DS(on)}$  is 12 mΩ at RT and 25 mΩ at 175°C, respectively. The measured device will be referred as device #1 in following sections.

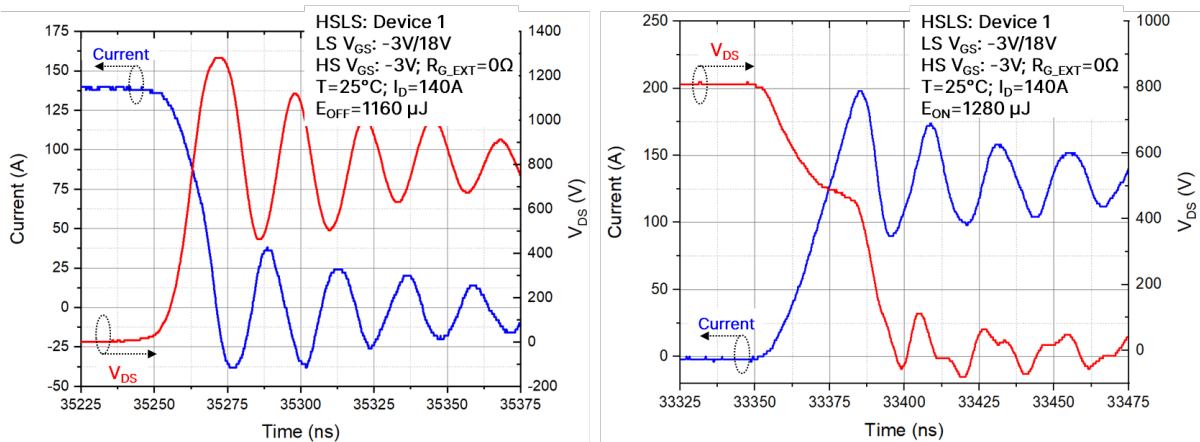


**Fig.1a.** Measured device #1 typical transfer characteristics at RT and 175°C, with  $V_{DS}=0.1V$ ;

**Fig. 1b.** Measured device #1 typical output characteristics at RT and 175°C, with  $V_{GS}=18V$ .

### Switching Characteristics

For switching evaluation, the same type of device as well as gate driver and  $R_{G\_EXT}$  was always used on both high side (HS) BD and low side (LS) switch. Fig. 2 show the measured switching turn-on and turn-off characteristics of the device #1 with  $I_D=140A$ , corresponding to  $J=700A/cm^2$ . Fast switching characteristics is observed where the devices turn-off  $I_D=140A$  in less than 20ns, and turn-on at  $di/dt \approx 6A/ns$  with extracted  $E_{OFF}=1160\mu J$  and  $E_{ON}=1280\mu J$ , respectively. The observed oscillations are difficult to avoid in the DPT system for these fast switching events.

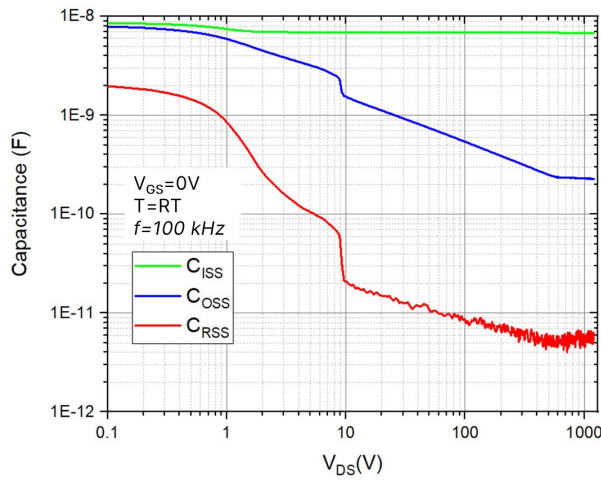


**Fig.2.** Measured device #1 switching characteristics in high current  $I_D=140A$  a) Turn-off;

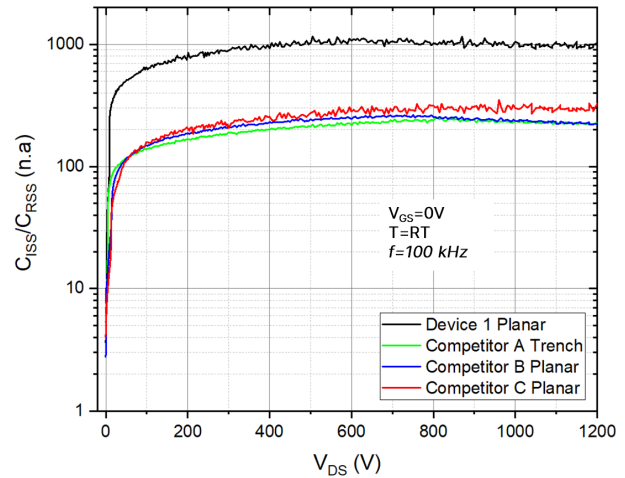
b) Turn-on.

## Capacitance-Voltage (C-V) Characteristics

As discussed, PTO occurs during HS BD turn-off and it is caused by the charging current of the reverse transfer capacitance  $C_{RSS}$  as it creates a voltage drop across the total gate resistance ( $R_{G\_INT} + R_{G\_EXT}$ ) and the input capacitances  $C_{ISS}$  [1, 2]. If the  $V_{GS}$  induced by this  $C_{RSS}$  charging event exceeds device's  $V_{TH}$ , then PTO is triggered in the HS MOSFET and creates additional BD “reverse recovery” current. PTO is therefore dependent on device capacitances like  $C_{RSS}$  and  $C_{ISS}$ , the total gate resistance ( $R_{G\_INT} + R_{G\_EXT}$ ), the switching speed,  $V_{TH}$ , and temperature. Fig.3a shows high voltage C-V characteristics of device #1 with good  $C_{ISS}/C_{RSS}$  ratios over a wide  $V_{DS}$  range. For comparing different devices, we present the area independent  $C_{ISS}/C_{RSS}$  ratio. Fig.3b displays measured  $C_{ISS}/C_{RSS}$  ratio of the devices #1 and three reference commercially available SiC MOSFETs. Device #1 shows significantly higher  $C_{ISS}/C_{RSS}$  ratio compared to the other devices for the whole  $V_{DS}$  range.



**Fig. 3a.** Measured C-V characteristics from device #1.



**Fig. 3b.** Measured  $C_{ISS}/C_{RSS}$  ratio of the devices considered in this work.

Other parameters that could affect device's PTO characteristics like devices  $R_{G\_INT}$  and  $V_{TH}$  as well as its RT  $R_{DS\_ON}$  were also listed in Table #1.

**Table 1.** Summary of measured  $R_{G\_INT}$  and  $V_{TH}$  as well as  $R_{DS\_ON}$  of device considered in this work

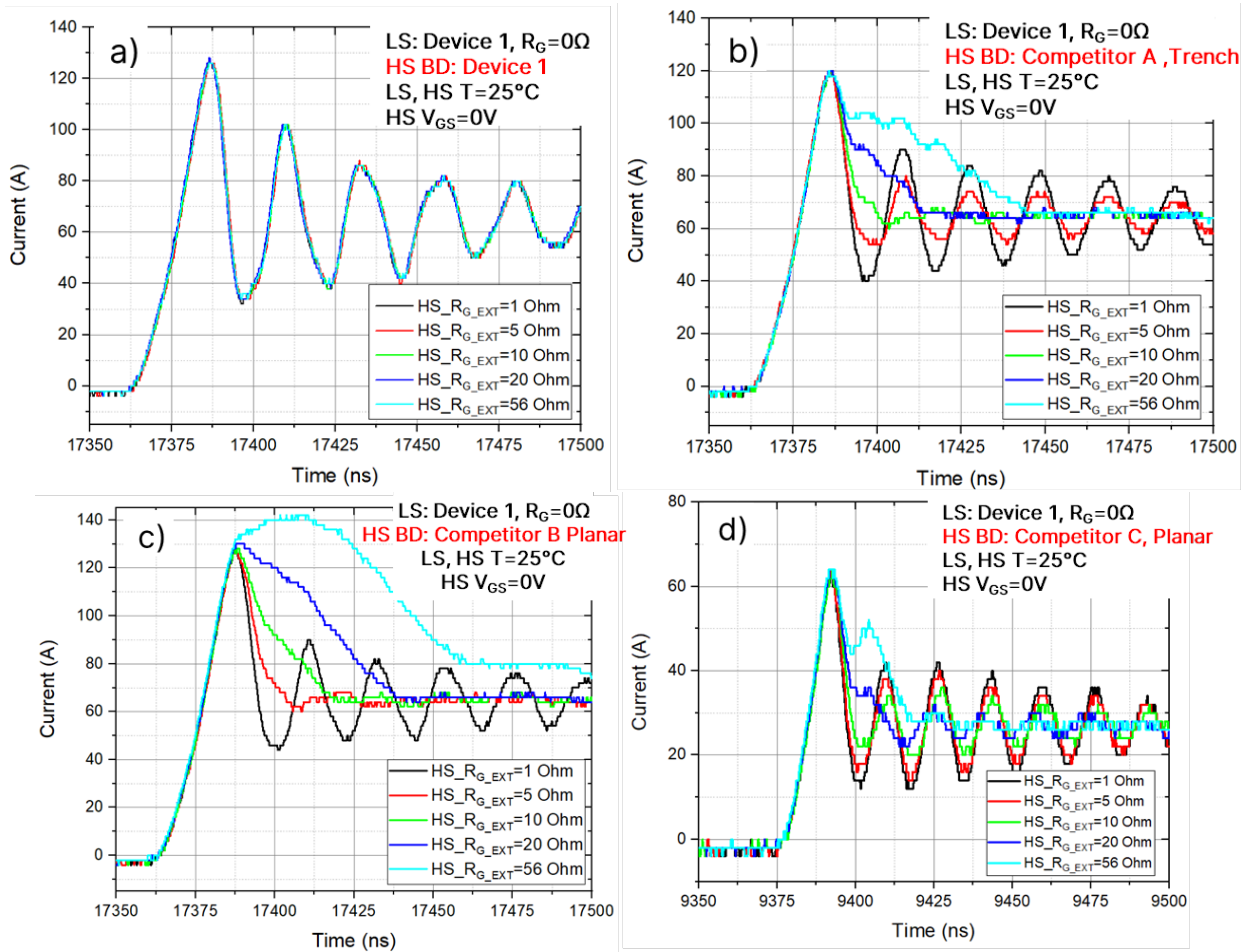
	Device #1	Competitor A Trench	Competitor B planar	Competitor C Planar
$R_{G\_INT} (\Omega) (@1 \text{ MHz})$	4.5	1.57	1.2	7.7
$V_{TH} (V)$	3	4.06	1.82	3.07
RT $R_{DS\_ON} (m\Omega)$	12	14	20	70

## Parasitic Turn-On

To investigate PTO, LS switch conditions (e.g.,  $V_{GS}$ , Temperature,  $R_{G\_EXT}$ ) were kept constant to maintain a fixed  $di/dt$ . HS  $V_{GS}=0V$  were applied and HS device were varied in HS  $R_{G\_EXT}$  and in temperature (from RT to 175°C).  $V_{DD}=800V$  were applied in this study.

Fig. 4a shows measured switching turn-on characteristics using the device #1 at RT as the HS BD, with different HS  $R_{G\_EXT}$ . No switching turn-on dependence on HS  $R_{G\_EXT}$  is observed even with very high HS  $R_{G\_EXT}$ . Same measurements with even higher  $R_{G\_EXT}$  up to few hundreds  $\Omega$  or device with even lower RT  $V_{TH}$ , e.g.,  $V_{TH}=2.1V$  also show almost no sign of PTO (data not shown).

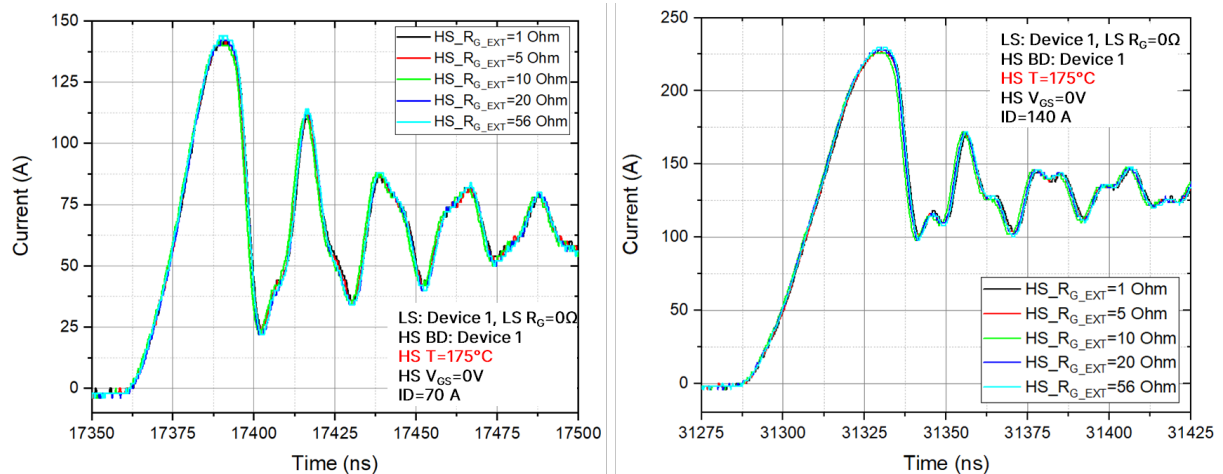
Fig. 4b-d) represent measured switching turn-on characteristics with different HS  $R_{G\_EXT}$ , using competitor A (trench), competitor B (planar) and competitor C (planar) as the HS BD at RT, respectively. Different degrees of PTO can be observed when using these devices as the HS BD. We believe the excellent  $C_{ISS}/C_{RSS}$  ratio as shown in Fig. 3b is the critical factor for the high immunity to PTO that is observed for the device #1, and that this  $C_{ISS}/C_{RSS}$  ratio is more important to suppress PTO than the  $V_{TH}$  level.



**Fig. 4.** Measured switching turn-on with HS  $R_{G\_EXT}$  variation for PTO evaluation by using different devices as the BD: a) Device #1; b) Competitor A Trench; c) Competitor B Planar; d) Competitor C Planar.

### High Temperature Parasitic Turn-On

Fig.5 displays measured turn-on characteristics vs.  $R_{G\_EXT}$  using device #1 as the HS BD at  $175^\circ\text{C}$ , at different current densities. At  $T=175^\circ\text{C}$  (with a lower  $V_{TH}$  compared to RT) at different current densities with  $V_{DD}=800\text{V}$  and a turn-on  $di/dt=6\text{A/ns}$ , no sign of PTO can be observed, even with a high  $R_{G\_EXT}=56\Omega$ . These results further highlight the strong immunity of device #1 against PTO.



**Fig. 5.** Measured switching turn-on with HS  $R_{G\_EXT}$  variation for PTO evaluation measured by using device 1 as the HS BD in  $T=175^\circ\text{C}$  with different current densities.

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## Summary

In this work, we demonstrated a 1200V planar SiC MOSFETs with low  $R_{ON}$ , competitive  $R_{SP}$ , fast switching characteristics and a superior  $C_{ISS}/C_{RSS}$  ratio. Thanks to its superior  $C_{ISS}/C_{RSS}$  ratio, the device is highly robust against PTO even under fast switching, high  $V_{DD}$ , high temperature and high  $R_{G\_EXT}$ .

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